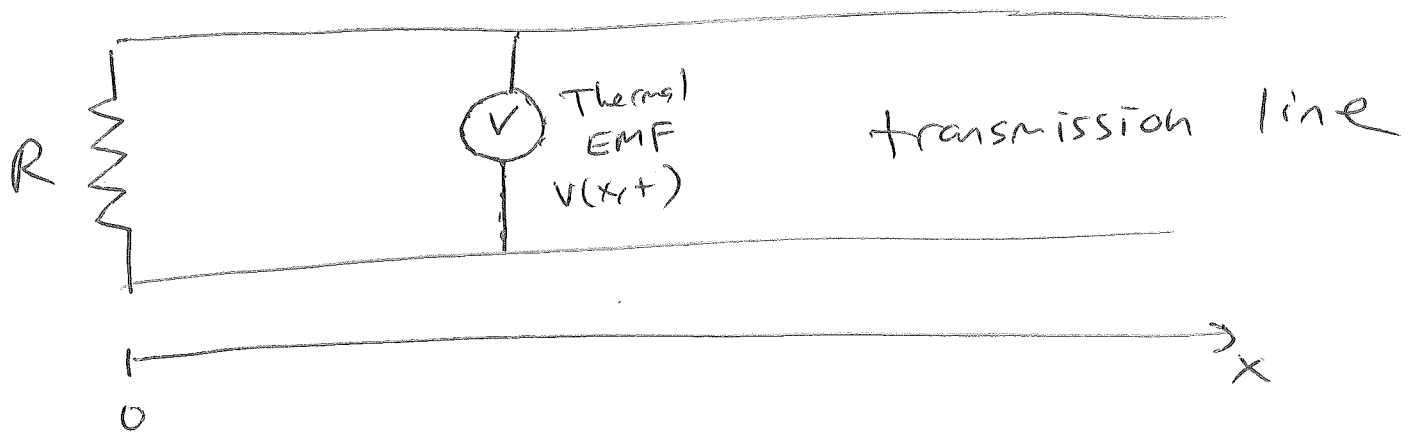
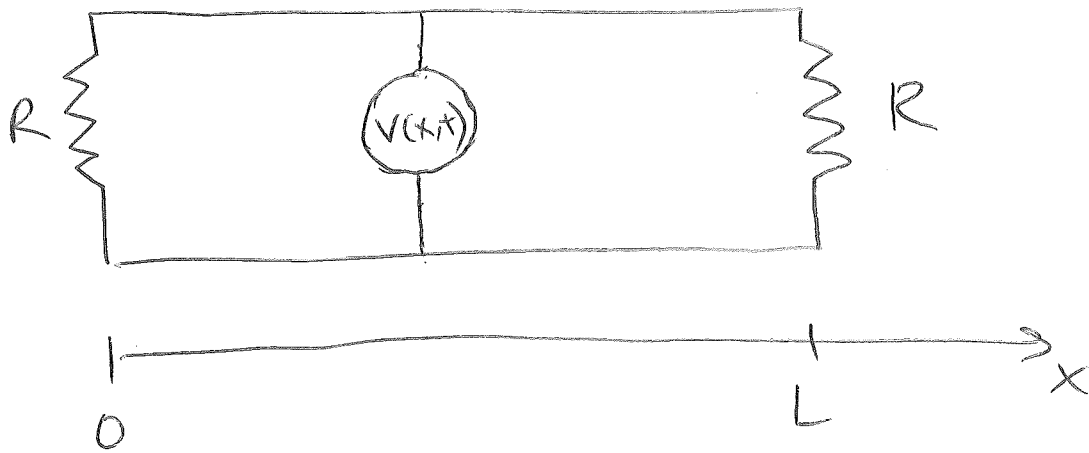


1) Johnson-Nyquist noise or 1D Blackbody radiation



Consider a long transmission line, of impedance $Z = R$, terminated by a resistor R . The system is in thermal equilibrium at temperature T .

The transmission line is like a one-dimensional cavity for EM waves. The resistor absorbs all waves incident upon it, and is therefore like a blackbody.



As far as our resistor on the left is concerned, the transmission line, terminated with a second resistor at $x=L$, looks the same as an infinite line, since R reflects nothing. The E+M waves in such a cavity satisfy Neumann boundary conditions:

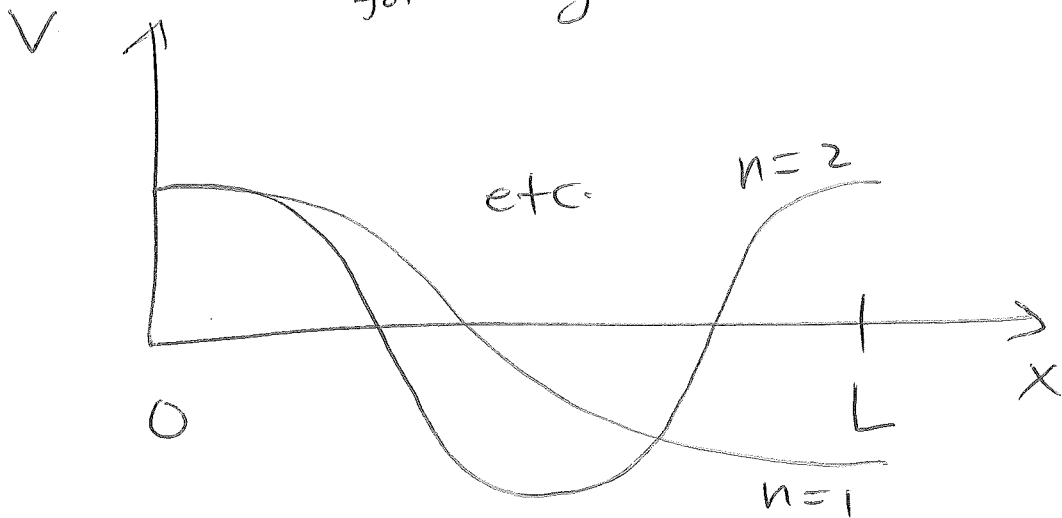
$$\left. \frac{\partial V}{\partial x} \right|_{x=0} = \left. \frac{\partial V}{\partial x} \right|_{x=L} = 0$$

The solutions are of the form

$$V(x,t) = V_0 \sin(\omega t + \phi) \cos\left(\frac{n\pi x}{L}\right)$$

for a given t :

11)



The wave equation for the transmission line is

$$\tilde{c}^2 \frac{\partial^2 V}{\partial x^2} = \frac{\partial^2 V}{\partial t^2},$$

where \tilde{c} is the speed of an E+M wave along the line. In general, $\tilde{c} \neq c$ due to the use of dielectrics between the two conductors.

$$\Rightarrow \tilde{c}^2 \left(\frac{n\pi}{L} \right)^2 = \omega^2$$

$$\omega_n = \frac{n\pi \tilde{c}}{L}$$

The thermal ave. occupancy of 112
mode n is

$$\langle S_n \rangle = \frac{1}{e^{\hbar \omega_n / T} - 1}$$

and the thermal average energy is

$$E = \sum_{n=1}^{\infty} \langle S_n \rangle \hbar \omega_n = \sum_{n=1}^{\infty} \frac{\hbar \omega_n}{e^{\hbar \omega_n / T} - 1}$$

$$\approx \int_0^{\infty} dn \frac{\hbar \omega_n}{e^{\hbar \omega_n / T} - 1} = \frac{\hbar L}{\pi \tilde{c}} \int_0^{\infty} d\omega \frac{\omega}{e^{\hbar \omega / T} - 1}$$

$$\equiv L \int_0^{\infty} d\omega u_\omega$$

u_ω = energy per unit length per unit
frequency in the transmission line.

$$u_\omega = \frac{\hbar \omega / \pi \tilde{c}}{e^{\hbar \omega / T} - 1}$$

The power absorbed by the resistor in the frequency range between ω and $\omega + d\omega$ is thus

$$P(\omega) d\omega = \tilde{c} \frac{u_{\omega}}{2} d\omega$$

(The factor of $\frac{1}{2}$ comes because half of the waves travel to the right and half travel left.)

$$P(\omega) = \frac{h\omega/2\pi}{e^{h\omega/T} - 1}$$

Since the resistor is matched to the impedance of the transmission line, it absorbs all power incident on it. In thermal equilibrium, the resistor must emit a power equal to that which it absorbs. (otherwise it would heat up or cool down.) This must be true in each frequency

interval, since we could insert a narrow-band filter between the resistor and the transmission line.

A resistor at temperature T must emit a power $P(\omega) = \frac{h\omega/2\pi}{e^{h\omega/T} - 1}$ per unit frequency. The total power emitted by the resistor is

$$P = \int_0^\infty d\omega P(\omega) = \int_0^\infty \frac{d\omega}{2\pi} \frac{h\omega}{e^{h\omega/T} - 1}$$

let $h\omega/T = x$

$$P = \frac{T^2}{h} \underbrace{\int_0^\infty dx \frac{x}{e^x - 1}}_I = \Gamma(2)\zeta(2) = \frac{\pi^2}{6}$$

$$I = \int_0^\infty dx \frac{x e^{-x}}{1 - e^{-x}} = \sum_{n=0}^\infty \int_0^\infty dx x e^{-x} (e^{-x})^n = \sum_{n=1}^\infty \underbrace{\int_0^\infty dx x e^{-nx}}_{\frac{1}{n^2}}$$
$$I = \sum_{n=1}^\infty \frac{1}{n^2} = \frac{\pi^2}{6}$$

⇒

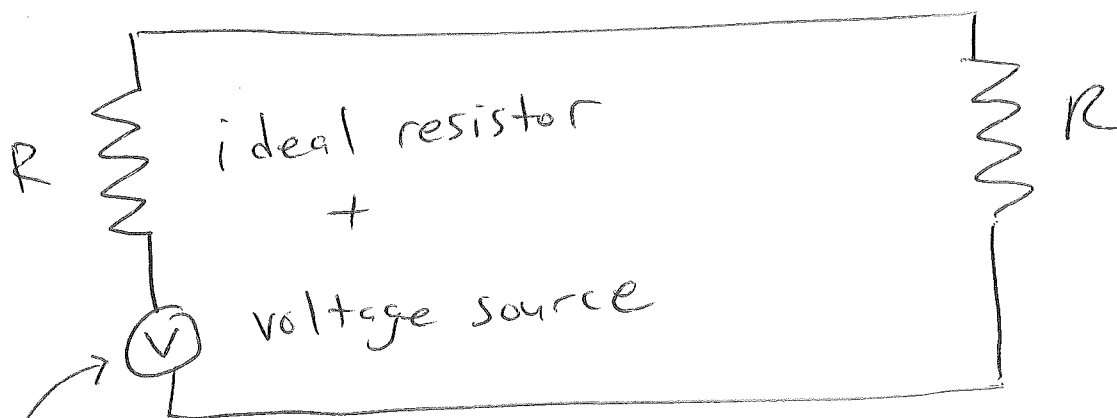
$$P = \frac{\pi^2 T^2}{6 h}$$

Current and voltage noise

$$P = \int_0^{\infty} d\omega \mathcal{P}(\omega) = \langle I^2 \rangle R$$

$\left[\begin{array}{l} \langle I \rangle = 0 \text{ in equilibrium, but} \\ \langle I^2 \rangle > 0 \end{array} \right]$

Equivalent circuit for noisy resistor:



This voltage source mimics the noise voltage in the real resistor.

From the equivalent circuit, it is clear that

$$V = 2R I$$

$$\langle I^2 \rangle R = \frac{\langle V^2 \rangle}{4R}$$

$$\begin{aligned} \langle V^2 \rangle &= 4R \int_0^{\infty} d\omega P(\omega) \\ &\equiv \int_0^{\infty} J_+(\omega) \frac{d\omega}{2\pi} \end{aligned}$$

$J_+(\omega)$ is the power spectrum of voltage fluctuations.

$$J_+(\omega) = 4R \frac{\hbar\omega}{e^{\hbar\omega/T} - 1}$$

Johnson-Nyquist noise

Classical limit $\hbar \rightarrow 0$
 ($\hbar\omega \ll T$)

$$J_{+}(\omega) \approx 4R \frac{\hbar\omega}{1 + \frac{\hbar\omega}{T} + \dots - 1}$$

$$J_{+}(\omega) \approx 4R T \quad T \gg \hbar\omega$$

This is an example of the
 "fluctuation-dissipation theorem."

The voltage fluctuations (V^2) are
 proportional to the coefficient R
 describing dissipation when a current
 flows.

$$\langle V(t) V(t) \rangle \equiv \int_0^{\infty} J_+(\omega) \frac{d\omega}{2\pi} = \int_{-\infty}^{\infty} J(\omega) \frac{d\omega}{2\pi}$$

$$\langle V(t) V(t+\tau) \rangle = \int_{-\infty}^{\infty} J(\omega) e^{i\omega\tau} \frac{d\omega}{2\pi}$$

$$J(\omega) = \int_{-\infty}^{\infty} d\tau \langle V(t) V(t+\tau) \rangle e^{-i\omega\tau}$$

$$J_+(\omega) = 2J(\omega)$$

$$\langle V^2 \rangle = \int_0^{\infty} \frac{d\omega}{2\pi} J_+(\omega) = 4R \int_0^{\infty} d\omega \rho(\omega)$$

$$= 4R \int_0^{\infty} \frac{d\omega}{2\pi} \frac{\hbar\omega}{e^{\beta\hbar\omega} - 1}$$

$$J_+(\omega) = \frac{4R \hbar\omega}{e^{\beta\hbar\omega} - 1}$$

$$\int_{-\infty}^{\infty} d\tau \langle V(t) V(t+\tau) \rangle e^{-i\omega\tau} = 2R \frac{\hbar\omega}{e^{\beta\hbar\omega} - 1}$$

$$J_+(\omega) \approx 4k_B T R \quad k_B T \gg \hbar \omega$$

$$\langle I^2 \rangle R = \int_0^\infty d\omega P(\omega)$$

$$\langle I^2 \rangle = G \int_0^\infty d\omega P(\omega)$$

Let

$$\langle I(t)I(t+\tau) \rangle = \int_{-\infty}^{\infty} \frac{d\omega}{2\pi} S(\omega) e^{i\omega\tau}$$

$$\langle I^2 \rangle = \int_{-\infty}^{\infty} \frac{d\omega}{2\pi} S(\omega) = \int_0^\infty \frac{d\omega}{2\pi} S_+(\omega)$$

$$= G \int_0^\infty d\omega P(\omega)$$

$$S_+(\omega) = G \frac{\hbar \omega}{e^{\beta \hbar \omega} - 1}$$

$$\approx G k_B T \quad \hbar \omega \ll k_B T$$

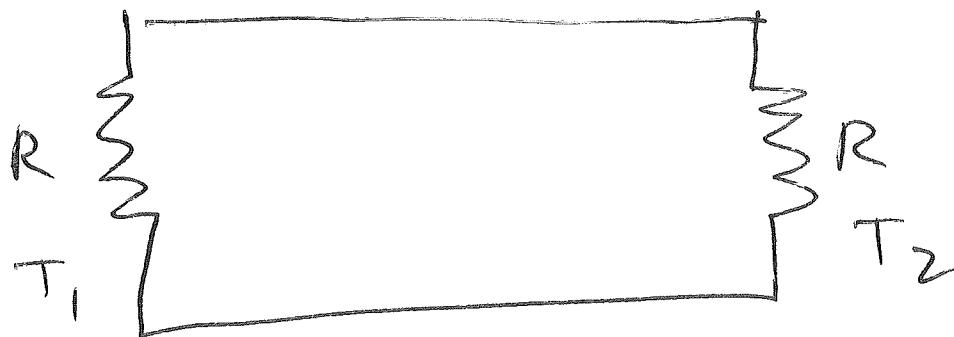
$$S_+(\omega) = 2S(\omega) = 2 \int_{-\infty}^{\infty} d\tau \langle I(t)I(t+\tau) \rangle e^{-i\omega\tau}$$

$$\int_{-\infty}^{\infty} d\tau \langle I(t)I(t+\tau) \rangle e^{-i\omega\tau} = G \frac{\hbar\omega/2}{e^{\beta\hbar\omega} - 1}$$

fluctuation-dissipation theorem

→ Relates equilibrium fluctuations
to dissipative response function
G (I = GV).

Quantum of Thermal Conductance



$$P_1 = \frac{\pi^2}{6} \frac{k_B^2 T_1^2}{h}, \quad P_2 = \frac{\pi^2}{6} \frac{k_B^2 T_2^2}{h}$$

$$I^Q = P_1 - P_2 = \frac{\pi^2}{6} \frac{k_B^2}{h} (T_1^2 - T_2^2)$$

$$= \frac{\pi^2}{3} \frac{k_B^2}{h} \left(\frac{T_1 + T_2}{2} \right) (T_1 - T_2)$$

$$= \left(\frac{\pi^2}{3} \frac{k_B^2}{h} T_0 \right) (T_1 - T_2)$$

$$K_0 = \frac{\pi^2}{3} \frac{k_B^2 T_0}{h} = \text{thermal conductance quantum}$$

= thermal conductance of a perfect 1D channel